



STUDENT ID NO

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# MULTIMEDIA UNIVERSITY

## FINAL EXAMINATION

**TRIMESTER 2, 2019/2020**

**EME4016 – HEAT TRANSFER**  
(ME)

28 FEBRUARY 2020  
3:00 p.m. – 5:00 p.m.  
(2 Hours)

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### INSTRUCTIONS TO STUDENTS

1. This Question Paper consists of six pages including the cover page and appendix.
2. Answer ALL four questions. Each question carries 25 marks and the distribution of the marks for each question is given in brackets [ ].
3. Write all your answers in the Answer Booklet provided.

### Question 1

(a) Consider one-dimensional steady heat conduction in a long solid cylinder of radius  $R$  and thermal conductivity  $k$  that contains a uniformly distributed heat source of  $\dot{q} \text{ W/m}^3$ . If the surface temperature is kept at a constant  $T_w$ , show that the temperature in the cylinder is given by

$$T = T_w + \frac{\dot{q}R^2}{4k} \left[ 1 - \left( \frac{r}{R} \right)^2 \right]$$

Take the applicable conduction equation in the cylinder as

$$\frac{k}{r} \frac{d}{dr} \left( r \frac{dT}{dr} \right) + \dot{q} = 0.$$

[10 marks]

(b) In one type of nuclear reactor the fuel elements consists of long cylindrical uranium rods sheathed or covered in thin light alloy tubes. These tubes are cooled by a stream of gas and the effective overall heat transfer coefficient from the uranium to the gas, based on the outside surface area, is  $900 \text{ W/m}^2 \cdot \text{K}$ . If the heat is generated uniformly in the uranium at the rate of  $2.0 \times 10^7 \text{ W/m}^3$  and if the coolant gas temperature is  $350^\circ\text{C}$ , estimate the rod diameter which gives a maximum permissible uranium temperature of  $600^\circ\text{C}$ . Take the thermal conductivity of uranium as  $29.8 \text{ W/m} \cdot \text{K}$ .

*Hint: Ignore the tube in your conduction analysis.*

[15 marks]

Continued...

### Question 2

(a) A metal slab of length  $0.1\text{ m}$  and width  $0.2\text{ m}$  is inserted at the center of a wooden plate of length  $0.5\text{ m}$  and width  $0.2\text{ m}$ . Consider a turbulent airstream at a temperature of  $20\text{ }^{\circ}\text{C}$  and a velocity of  $10\text{ m/s}$  that flows over the entire length of the plate. A heat source is attached to the lower side of the plate to maintain isothermal condition over the entire plate. (Please refer to the appendix for the properties table)

(i) Determine the total heat transfer rate that transferred to the metal slab in order to maintain the metal slab surface temperature at constant  $50\text{ }^{\circ}\text{C}$ . [10 marks]

(ii) If the air blower that maintains the airstream velocity is malfunctions, but other conditions remain unchanged as stated in the question, estimate the surface temperature of the metal slab and explain if the estimated value can be accepted.

*Hint: Assume a film temperature.* [15 marks]

Table Q2: Nusselt number correlations

| Correlation                         | Conditions   |
|-------------------------------------|--|
| $Nu_x = 0.332 Re_x^{1/2} Pr^{1/3}$  | Laminar flow   |
| $Nu_x = 0.0296 Re_x^{4/5} Pr^{1/3}$ | Turbulent flow   |
| $\overline{Nu} = 0.54 Ra_L^{1/4}$   | $10^4 \leq Ra_L \leq 10^7$ ; $L \equiv \frac{A_s}{P}$    |
| $\overline{Nu} = 0.15 Ra_L^{1/3}$   | $10^7 \leq Ra_L \leq 10^{11}$ ; $L \equiv \frac{A_s}{P}$ |

Continued...

**Question 3**

(a) A long circular aluminum fin is attached at one end to a heated wall and transfers heat by convection to a cold fluid.

(i) Obtain an expression to describe the heat transfer rate from the fin. *Hint: Please utilize the given fin temperature profile.*

$$\frac{T(x) - T_{\infty}}{T_b - T_{\infty}} = e^{-mx}$$

[5 marks]

(ii) With reference to the answer obtained from part (i), How much would the heat transfer rate be enhanced if the diameter of the fin is doubled? [4 marks]

(b) A cross flow heat exchanger is used in a cardiopulmonary bypass procedure to cool the blood flowing at a rate of 6000 ml per minute from a body temperature of 37 °C to 25 °C, to induce body hypothermia. Ice water at 0 °C is applied as a coolant and its outlet temperature is expected to be 20 °C. Both the blood and the ice water are unmixed. The overall heat transfer coefficient is 750 W/m<sup>2</sup>K. The blood properties are given as  $\rho = 1050 \text{ kg/m}^3$  and  $C_p = 3740 \text{ J/kg.K}$ . The water properties are given as  $\rho = 1000 \text{ kg/m}^3$  and  $C_p = 4198 \text{ J/kg.K}$ .

(i) Determine the volumetric flow rate of the water. [8 marks]

(ii) Determine the effectiveness of the heat exchanger. [5 marks]

(iii) The overall heat transfer coefficient of the cross flow heat exchanger used in a cardiopulmonary bypass reduces with time. Name this phenomenon and identify the possible factors. [3 marks]

**Continued...**

**Question 4**

(a) Define the view (or shape) factor  $F_{1-2}$  for radiation from body 1 to body 2. What is its relation to the complementary factor  $F_{2-1}$ ?

[4 marks]

(b) A special furnace is in the shape of a long triangular section channel. If the shape of the triangle is equilateral, show that the view factor between any two sides is 0.5. If the triangle is not equilateral, find an expression for  $F_{1-2}$  in terms of the side areas  $A_1, A_2$  and  $A_3$ , for sides 1, 2, and 3, respectively. Hence evaluate  $F_{1-2}$  in the case of  $A_1 = 5 \text{ m}^2, A_2 = 4 \text{ m}^2$  and  $A_3 = 3 \text{ m}^2$ .

[10 marks]

(c) A convex body of surface area  $1 \text{ m}^2$ , emissivity 0.8 and temperature  $900 \text{ K}$  is totally enclosed by a body of surface area  $3 \text{ m}^2$ , emissivity 0.7 and temperature  $700 \text{ K}$ . Evaluate the net radiative heat transfer rate between these bodies. Take the Stefan-Boltzmann constant as  $5.67 \times 10^{-8} \text{ W/m}^2 \cdot \text{K}^4$ .

[11 marks]

**Continued...**

## Appendix: Properties of air at 1 atm pressure

Properties of air at 1 atm pressure

| Temp.,<br><i>T</i> , °C | Density,<br><i>ρ</i> , kg/m <sup>3</sup> | Specific<br>Heat,<br><i>C<sub>p</sub></i> , J/kg · °C | Thermal<br>Conductivity,<br><i>k</i> , W/m · °C | Thermal<br>Diffusivity,<br><i>α</i> , m <sup>2</sup> /s | Dynamic<br>Viscosity,<br><i>μ</i> , kg/m · s | Kinematic<br>Viscosity,<br><i>ν</i> , m <sup>2</sup> /s | Prandtl<br>Number,<br><i>Pr</i> |
|-------------------------|--|---|---|---|--|---|---------------------------------|
| -150                    | 2.866                                    | 983   | 0.01171   | 4.158 × 10 <sup>-6</sup>                                | 8.636 × 10 <sup>-8</sup>                     | 3.013 × 10 <sup>-6</sup>                                | 0.7246                          |
| -100                    | 2.038                                    | 966   | 0.01582   | 8.036 × 10 <sup>-6</sup>                                | 1.189 × 10 <sup>-6</sup>                     | 5.837 × 10 <sup>-6</sup>                                | 0.7263                          |
| -50                     | 1.582                                    | 999   | 0.01979   | 1.252 × 10 <sup>-5</sup>                                | 1.474 × 10 <sup>-5</sup>                     | 9.319 × 10 <sup>-6</sup>                                | 0.7440                          |
| -40                     | 1.514                                    | 1002  | 0.02057   | 1.356 × 10 <sup>-5</sup>                                | 1.527 × 10 <sup>-5</sup>                     | 1.008 × 10 <sup>-5</sup>                                | 0.7436                          |
| -30                     | 1.451                                    | 1004  | 0.02134   | 1.465 × 10 <sup>-5</sup>                                | 1.579 × 10 <sup>-5</sup>                     | 1.087 × 10 <sup>-5</sup>                                | 0.7425                          |
| -20                     | 1.394                                    | 1005  | 0.02211   | 1.578 × 10 <sup>-5</sup>                                | 1.630 × 10 <sup>-5</sup>                     | 1.169 × 10 <sup>-5</sup>                                | 0.7408                          |
| -10                     | 1.341                                    | 1006  | 0.02288   | 1.696 × 10 <sup>-5</sup>                                | 1.680 × 10 <sup>-5</sup>                     | 1.252 × 10 <sup>-5</sup>                                | 0.7387                          |
| 0                       | 1.292                                    | 1006  | 0.02364   | 1.818 × 10 <sup>-5</sup>                                | 1.729 × 10 <sup>-5</sup>                     | 1.338 × 10 <sup>-5</sup>                                | 0.7362                          |
| 5                       | 1.269                                    | 1006  | 0.02401   | 1.880 × 10 <sup>-5</sup>                                | 1.754 × 10 <sup>-5</sup>                     | 1.382 × 10 <sup>-5</sup>                                | 0.7350                          |
| 10                      | 1.246                                    | 1006  | 0.02439   | 1.944 × 10 <sup>-5</sup>                                | 1.778 × 10 <sup>-5</sup>                     | 1.426 × 10 <sup>-5</sup>                                | 0.7336                          |
| 15                      | 1.225                                    | 1007  | 0.02476   | 2.009 × 10 <sup>-5</sup>                                | 1.802 × 10 <sup>-5</sup>                     | 1.470 × 10 <sup>-5</sup>                                | 0.7323                          |
| 20                      | 1.204                                    | 1007  | 0.02514   | 2.074 × 10 <sup>-5</sup>                                | 1.825 × 10 <sup>-5</sup>                     | 1.516 × 10 <sup>-5</sup>                                | 0.7309                          |
| 25                      | 1.184                                    | 1007  | 0.02551   | 2.141 × 10 <sup>-5</sup>                                | 1.849 × 10 <sup>-5</sup>                     | 1.562 × 10 <sup>-5</sup>                                | 0.7296                          |
| 30                      | 1.164                                    | 1007  | 0.02588   | 2.208 × 10 <sup>-5</sup>                                | 1.872 × 10 <sup>-5</sup>                     | 1.608 × 10 <sup>-5</sup>                                | 0.7282                          |
| 35                      | 1.145                                    | 1007  | 0.02625   | 2.277 × 10 <sup>-5</sup>                                | 1.895 × 10 <sup>-5</sup>                     | 1.655 × 10 <sup>-5</sup>                                | 0.7268                          |
| 40                      | 1.127                                    | 1007  | 0.02662   | 2.346 × 10 <sup>-5</sup>                                | 1.918 × 10 <sup>-5</sup>                     | 1.702 × 10 <sup>-5</sup>                                | 0.7255                          |
| 45                      | 1.109                                    | 1007  | 0.02699   | 2.416 × 10 <sup>-5</sup>                                | 1.941 × 10 <sup>-5</sup>                     | 1.750 × 10 <sup>-5</sup>                                | 0.7241                          |
| 50                      | 1.092                                    | 1007  | 0.02735   | 2.487 × 10 <sup>-5</sup>                                | 1.963 × 10 <sup>-5</sup>                     | 1.798 × 10 <sup>-5</sup>                                | 0.7228                          |
| 60                      | 1.059                                    | 1007  | 0.02808   | 2.632 × 10 <sup>-5</sup>                                | 2.008 × 10 <sup>-5</sup>                     | 1.896 × 10 <sup>-5</sup>                                | 0.7202                          |
| 70                      | 1.028                                    | 1007  | 0.02881   | 2.780 × 10 <sup>-5</sup>                                | 2.052 × 10 <sup>-5</sup>                     | 1.995 × 10 <sup>-5</sup>                                | 0.7177                          |
| 80                      | 0.9994                                   | 1008  | 0.02953   | 2.931 × 10 <sup>-5</sup>                                | 2.096 × 10 <sup>-5</sup>                     | 2.097 × 10 <sup>-5</sup>                                | 0.7154                          |
| 90                      | 0.9718                                   | 1008  | 0.03024   | 3.086 × 10 <sup>-5</sup>                                | 2.139 × 10 <sup>-5</sup>                     | 2.201 × 10 <sup>-5</sup>                                | 0.7132                          |
| 100                     | 0.9458                                   | 1009  | 0.03095   | 3.243 × 10 <sup>-5</sup>                                | 2.181 × 10 <sup>-5</sup>                     | 2.306 × 10 <sup>-5</sup>                                | 0.7111                          |
| 120                     | 0.8977                                   | 1011  | 0.03235   | 3.565 × 10 <sup>-5</sup>                                | 2.264 × 10 <sup>-5</sup>                     | 2.522 × 10 <sup>-5</sup>                                | 0.7073                          |
| 140                     | 0.8542                                   | 1013  | 0.03374   | 3.898 × 10 <sup>-5</sup>                                | 2.345 × 10 <sup>-5</sup>                     | 2.745 × 10 <sup>-5</sup>                                | 0.7041                          |
| 160                     | 0.8148                                   | 1016  | 0.03511   | 4.241 × 10 <sup>-5</sup>                                | 2.420 × 10 <sup>-5</sup>                     | 2.975 × 10 <sup>-5</sup>                                | 0.7014                          |
| 180                     | 0.7788                                   | 1019  | 0.03646   | 4.593 × 10 <sup>-5</sup>                                | 2.504 × 10 <sup>-5</sup>                     | 3.212 × 10 <sup>-5</sup>                                | 0.6992                          |
| 200                     | 0.7459                                   | 1023  | 0.03779   | 4.954 × 10 <sup>-5</sup>                                | 2.577 × 10 <sup>-5</sup>                     | 3.455 × 10 <sup>-5</sup>                                | 0.6974                          |
| 250                     | 0.6746                                   | 1033  | 0.04104   | 5.890 × 10 <sup>-5</sup>                                | 2.760 × 10 <sup>-5</sup>                     | 4.091 × 10 <sup>-5</sup>                                | 0.6946                          |
| 300                     | 0.6158                                   | 1044  | 0.04418   | 6.871 × 10 <sup>-5</sup>                                | 2.934 × 10 <sup>-5</sup>                     | 4.765 × 10 <sup>-5</sup>                                | 0.6935                          |
| 350                     | 0.5664                                   | 1056  | 0.04721   | 7.892 × 10 <sup>-5</sup>                                | 3.101 × 10 <sup>-5</sup>                     | 5.475 × 10 <sup>-5</sup>                                | 0.6937                          |
| 400                     | 0.5243                                   | 1069  | 0.05015   | 8.951 × 10 <sup>-5</sup>                                | 3.261 × 10 <sup>-5</sup>                     | 6.219 × 10 <sup>-5</sup>                                | 0.6948                          |
| 450                     | 0.4880                                   | 1081  | 0.05298   | 1.004 × 10 <sup>-4</sup>                                | 3.415 × 10 <sup>-5</sup>                     | 6.997 × 10 <sup>-5</sup>                                | 0.6965                          |
| 500                     | 0.4565                                   | 1093  | 0.05572   | 1.117 × 10 <sup>-4</sup>                                | 3.563 × 10 <sup>-5</sup>                     | 7.805 × 10 <sup>-5</sup>                                | 0.6986                          |
| 600                     | 0.4042                                   | 1115  | 0.06093   | 1.352 × 10 <sup>-4</sup>                                | 3.846 × 10 <sup>-5</sup>                     | 9.515 × 10 <sup>-5</sup>                                | 0.7037                          |
| 700                     | 0.3627                                   | 1135  | 0.06581   | 1.598 × 10 <sup>-4</sup>                                | 4.111 × 10 <sup>-5</sup>                     | 1.133 × 10 <sup>-4</sup>                                | 0.7092                          |
| 800                     | 0.3289                                   | 1153  | 0.07037   | 1.855 × 10 <sup>-4</sup>                                | 4.362 × 10 <sup>-5</sup>                     | 1.326 × 10 <sup>-4</sup>                                | 0.7149                          |
| 900                     | 0.3008                                   | 1169  | 0.07465   | 2.122 × 10 <sup>-4</sup>                                | 4.600 × 10 <sup>-5</sup>                     | 1.529 × 10 <sup>-4</sup>                                | 0.7206                          |
| 1000                    | 0.2772                                   | 1184  | 0.07868   | 2.398 × 10 <sup>-4</sup>                                | 4.826 × 10 <sup>-5</sup>                     | 1.741 × 10 <sup>-4</sup>                                | 0.7260                          |
| 1500                    | 0.1990                                   | 1234  | 0.09599   | 3.908 × 10 <sup>-4</sup>                                | 5.817 × 10 <sup>-5</sup>                     | 2.922 × 10 <sup>-4</sup>                                | 0.7478                          |
| 2000                    | 0.1553                                   | 1264  | 0.11113   | 5.664 × 10 <sup>-4</sup>                                | 6.630 × 10 <sup>-5</sup>                     | 4.270 × 10 <sup>-4</sup>                                | 0.7539                          |

Note: For ideal gases, the properties  $C_p$ ,  $k$ ,  $\mu$ , and  $Pr$  are independent of pressure. The properties  $\rho$ ,  $\nu$ , and  $\alpha$  at a pressure  $P$  (in atm) other than 1 atm are determined by multiplying the values of  $\rho$  at the given temperature by  $P$  and by dividing  $\nu$  and  $\alpha$  by  $P$ .

Source: Data generated from the EES software developed by S. A. Klein and F. L. Alvarado. Original sources: Keenan, Chap, Keyes, Gas Tables, Wiley, 198; and Thermophysical Properties of Matter, Vol. 3: Thermal Conductivity, Y. S. Touloukian, P. E. Liley, S. C. Saxena, Vol. 11: Viscosity, Y. S. Touloukian, S. C. Saxena, and P. Hostermans, IFI/Plenum, NY, 1970, ISBN 0-306057020-8.

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